

TOKAPOLE MONITOR SYSTEM

J.C. Sprott

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Introduction

For many years a Radio Shack Model I, Level II, 16 K TRS-80 with a Connecticut Microcomputer Model AIM16, 8 bit, 16 channel, 100 μ sec A-to-D converter has been used to monitor standard machine and discharge parameters on Tokapole II. The system has slowly evolved over the years, but has remained relatively unchanged for the past year. It is appropriate, therefore, to document the system in its present form for those who need to understand how it works. The documentation here applies to the 26 Jan 83 version of the software and is subject to change if improvements are made. A compiled version of the program is also available, dated 28 Jan 83, and differs only in minor details such as timing loops. It runs at about five times the speed of the BASIC version.

Loading Instructions (BASIC version)

1) Make sure the computer and video display are ON. The computer is turned on by a push-button on the rear of the keyboard next to the three plugs that attach to the cassette and video display. The computer is ON when the red LED on the keyboard is illuminated. The computer powers up with the question MEM SIZE?__. You can cause the computer to initialize itself and ask the MEM SIZE question from BASIC by typing:

SYSTEM <ENTER>

/ ϕ <ENTER>

(<ENTER> means press the white ENTER key.) The MEM SIZE question allows you to reserve memory for use of machine language programs. Although the TOKAPOLE MONITOR program requires 767 bytes of reserved memory

(MEM SIZE = 32000), this is done automatically by the program, and therefore one need only press <ENTER> in response to this question. The computer should respond with

READY

>_

to indicate that it will now accept BASIC commands.

2)Place the cassette tape labeled TOKAPOLE MONITOR in the recorder and rewind. Press the PLAY button on the recorder and type CLOAD <ENTER>. Within about 5 seconds a pair of flashing astericks will appear in the upper right corner of the screen indicating that the program is loading. If the astericks fail to appear or do not blink, the volume is probably set wrong on the recorder, or the plugs are not inserted, or the tape is defective. A backup version of the program is located a little further along (counter setting 050) on the same tape. When loading is complete (after about 1-1/2 minutes), the recorder will stop. Rewind the tape and put it away. It is no longer needed. Type RUN <ENTER> to cause the program to run. It will identify itself and request a baseline shot (a machine shot without plasma). Before it runs, it performs a memory check to see if the correct number of bytes was loaded and gives an error message, MEMORY CHECK ERROR ON LOAD, if it detects a problem. If this happens, start over. A BASIC listing of the program is included in Appendix A.

Loading Instructions (Compiled version)

1)Make sure the computer and video display are ON and enter BASIC as described in 1) above.

2)Place the cassette tape labeled TOKMON in the recorder and rewind. Press the PLAY button on the recorder and type

SYSTEM <ENTER>

TOKMON <ENTER>

The astericks in the upper right corner will flash, but more slowly than with the BASIC version. When the tape stops (after about 3-1/3 minutes), rewind and put it away. Then type

/ <ENTER>

RUN <ENTER>

The program will identify itself and run as before, except at five times the speed.

3) If you interrupt the program by pressing the <BREAK> key, you normally cannot continue by typing CONT <ENTER> as with a BASIC program. You will have to type RUN <ENTER>, and all previous data will be lost. You can LIST the program, but you won't see anything very interesting. You cannot EDIT or add anything to the program. Attempting to do so will likely necessitate reloading the program from scratch.

Running the Program

The program is intended to run unattended. The default option is for the program to display plasma current (I_p), ion saturation current density (J_{SAT}), toroidal field (B_T), poloidal gap voltage (V_{PG}), hoop current (I_H), and the time derivative of the plasma current (dI_p/dt) for the first 10 msec after the poloidal field is fired. It does this immediately after the shot and then rearms itself and waits for the next shot as indicated by a single illuminated pixel in the upper right corner of the video display. When it receives a trigger, a second adjacent pixel will illuminate. Other command sequences can be programmed by pressing the P key. Most of these are obvious or can be learned by trial and error. A command sequence is a series of letters and numbers indicating the sequence in which the various

commands are performed. A single digit between 1 and 9 will cause a delay of the corresponding number of seconds. For example, the command sequence 5I5J5L5A <ENTER> will cause the default data table, the plasma current graph, the ion saturation current graph, the amp-seconds for the previous shots, and the table of additional derived data to be displayed in sequence with a five second delay between each. For longer delays one can use, for example, 999 which will cause a 27 second delay.

Otherwise, the only attention the program requires is to take a new baseline when requested. The program determines this by comparing the measured plasma current at 20 msec (which it assumes should be zero) with the baseline signal. If the difference exceeds 9 kA, all successive shots will request a baseline, and the data should be interpreted with caution until a new baseline is taken. When the measured plasma current at 20 msec is not zero, the computer assumes that the error is due to a change in hoop temperature and adjusts the displayed currents accordingly, so that the current indicated by the computer will always read within 1 kA of zero at 20 msec. The computer recognizes a baseline if the sum of the ion saturation current density at 2.5, 5.0, and 7.5 msec is less than 50 mA/cm^2 . During a run, the plasma current baseline will slowly drift downward as the hoops heat up, changing their resistance, but the computer will correct for this up to a point. The seriousness of this effect will depend on the poloidal field strength and the recycle time. It is also generally impossible to get a good baseline at normal poloidal field strengths without using the core cocking circuit because the iron core saturates before 20 msec at a slightly different time with and without the plasma. When making careful measurements, it is advisable to retake a baseline whenever

any of the capacitor bank voltages is altered even though the computer's criterion for needing a baseline may not be met.

What the Program Does

When the program is ready to receive data (pixel in the upper right corner illuminated), the V_{PG} channel is being interrogated every 100 μ sec by a machine language software loop (see Appendix B). Whenever the highest order bit becomes a one (>127), the five channels (I_P , J_{SAT} , B_T , V_{PG} , and I_H) are read in sequence at a rate of 100 μ sec each for a total time of 20 msec, thereby generating 200 values which are stored in a two-dimensional array with dimensions $X(5,40)$. The baseline is similarly stored in an array $XB(5,40)$. The value of a quantity I is determined at time step J from

$$S(I,J) = SC(I) * (X(I,J) - XB(I,J))$$

where $SC(I)$ is a scale factor for that particular channel to make the units come out as follows:

<u>quantity</u>	<u>scale factor</u>	<u>units</u>
I_P	$SC(1)=1$	kA
J_{SAT}	$SC(2)=10$	mA/cm ²
B_T	$SC(3)=200$	gauss
V_{PG}	$SC(4)=0.5$	volts
I_H	$SC(5)=2$	kA

The scale factor can also be thought of as the smallest measurable increment of the corresponding quantity. Actually, in order to determine the quantities at a given time (such as 4 msec), the values are interpolated from the one just below and just above the desired time. The first measurement of I_P occurs at $t=0.1$ msec, the first measurement of J_{SAT} occurs at $t=0.2$ msec, etc. The second measurement of I_P occurs at $t=0.6$ msec, etc. Note that the trigger scheme introduces a 100 μ sec jitter into the timing,

and that there is a threshold trigger level, but neither of these has ever been a serious problem. A sixth channel, neutral pressure, is read from the fast ion gauge just after the 20 msec point and compared with a baseline pressure just before the A-to-D is rearmed. This reading has not proved very reliable or useful because the I_p channel is often saturated at that time, resulting in erroneous pressure readings.

Whenever the absolute value of the measured plasma current at 20 msec exceeds 1 kA, the computer assumes the plasma current baseline has drifted due to a change in hoop resistance and adjusts the measured current by subtracting from it a quantity,

$$\Delta I_p(t) = I_p(20) \int_0^t I_H dt / \int_0^{20} I_H dt \quad (1)$$

where t is in milliseconds. The justification for this correction is given by Eq. (12). Although the computer will continue to track a drift in resistance indefinitely, whenever the unadjusted current at 20 msec, $|I_p(20)|$ exceeds 9 kA, a baseline is requested.

The program calculates the amp-seconds (a figure of merit for the discharge) by numerically integrating the plasma current:

$$AS = \int_0^{20} I_p dt \quad (2)$$

where I_p is in kA and t is in milliseconds. If the plasma current is negative, it is set to zero in the above integral to reduce the effect of an erroneous baseline. Whenever a baseline is needed, the amp-seconds is not calculated but rather set to zero to avoid meaningless readings.

From the measured quantities, several additional derived data can be displayed (using the A command). An effective minor radius of the plasma (in cm) is calculated from

$$a = 17.4 |I_P/I_H|^{1/4} \quad (3)$$

This radius is meant to be the radius of a circle of the same cross-sectional area as that enclosed by the square-shaped plasma inside the separatrix. This quantity is only approximate because of a number of assumptions, the most serious of which is that the entire measured current flows in a circularly symmetric fashion within a circle of radius a centered on the geometric axis of the machine. It also assumes a degenerate octupole field in the absence of plasma, such that in the vicinity of the field nulls the octupole field varies like r^3 .

The average safety factor $\langle q \rangle$ is determined by assuming that the plasma current density is uniform over the cross-section of a circle of radius a centered on the axis. The current density is then independent of radius, and $\langle q \rangle$ is constant out to a radius at which the octupole field starts to compare with the plasma field (near the separatrix). Near the axis the $\langle q \rangle$ is given by

$$\langle q \rangle = 10^{-4} a^2 B_T / I_P \quad (4)$$

Calculation of the loop voltage V_ℓ is considerably more difficult. To begin with, we mean by loop voltage only the resistive part of the voltage applied to the plasma, i.e.: the voltage that would be measured by a single turn loop of wire that goes once around the machine toroidally at the magnetic axis. Other tokamaks measure loop voltage by a toroidal loop at

the plasma edge, and hence there is a contribution to the measured signal from the time derivative of the poloidal magnetic flux in the plasma. The loop voltage can be expressed in terms of the measured quantities (I_P , V_{PG} , and I_H) using the circuit model of PLP 777:

$$V_\ell = \alpha V_{PG} + (1-\alpha)R_H I_H - \alpha(1-\alpha)L_H \frac{dI_P}{dt} - \frac{d}{dt}(L_P I_P) \quad (5)$$

where α =private flux/common flux in the absence of a plasma (typically 0.5), R_H is the hoop resistance, L_H is the hoop inductance, and L_P is the plasma inductance. This equation differs from Eq. (7) of PLP 756 in that the sign of the $L_H dI_P/dt$ term is opposite. The reason is that the plasma inductance is here defined so as to include the image currents of the plasma in the hoops, i.e.: the hoops represent a conducting boundary which alters the plasma inductance. In PLP 756, the plasma inductance is calculated as if the hoops were absent. This difference is of little consequence, however, since the plasma inductance L_P cannot be measured directly, but rather the quantity $L_P + \alpha(1-\alpha)L_H$ (as defined above) is measured as described in PLP 756 to have a value of $\sim 0.7 \mu\text{H}$. The term $I_P dL_P/dt$ cannot be easily measured and undoubtedly gives rise to some high frequency structure on the loop voltage, but it is thought to be unimportant for the low frequency components of V_ℓ . Actually, the method of determining the plasma inductance by experimentally measuring $dV_\ell/d\dot{I}_P$ takes into account that portion of the $I_P dL_P/dt$ that results from a simple expansion or contraction of the plasma radius a in response to a change in I_P . Current profile changes are not modelled properly, however. The quantities α and R_H can be estimated theoretically, but since they change in time due to soak-in, a better representation was obtained by Sprott and Shepard by measuring the loop voltage directly as

described in PLP 756 in the absence of plasma and then fitting the results to a function of the form

$$V_{\ell} = \frac{1}{2}(1+At)V_{PG} + B(1+Ct)I_H \quad (6)$$

where A, B, and C are constants. Such a method gives a first-order correction to the time dependence of α and R_H as well as the initial value of R_H . The data (45 points) were taken at 2 msec intervals up to 20 msec for a crowbarred, damped poloidal field waveform for a variety of poloidal bank and power crowbar settings. Similarly, the effect of \dot{I}_p on the loop voltage was determined by measuring the loop voltage difference ΔV_{ℓ} with and without a plasma using a probe on axis as described above. The data (20 points) were taken at 0.5 msec intervals for several 4 msec discharges with peak current of ~ 25 kA at 1.5 msec and fitted to a curve of the form $\Delta V_{\ell} = -Aa^B \dot{I}_p$ over the range $7 < a < 11$ cm. The fit was not excellent but gave $A=2.3$ and $B=-0.5$. This method undoubtedly hides a multitude of sins, and it should be redone more carefully. Nevertheless, the values obtained give

$$V_{\ell} = \frac{1}{2}(1+t/75)V_{PG} + 0.0045(1-t/37)I_H - 2.3\dot{I}_p/\sqrt{a} \quad (7)$$

where t is the time in msec after the start of the poloidal voltage pulse, and the currents are measured in kiloamps. Calculation of the time derivative of the plasma current \dot{I}_p poses some special problems. The plasma current trace is not perfectly smooth, and the differentiated value of the wiggles can overwhelm the low frequency signal that is thought to be of primary interest. After much experimentation a method was settled upon in which a parabola is fit to the four I_p points nearest the time of interest

(spanning a 1.5 msec interval), and the derivative at the desired point is determined analytically from the parabola. The round-off error in the A-to-D converter gives an rms error in the loop voltage measurement of ± 0.5 volts which is considerable since our standard discharges have V_ℓ in the range of 2-3 volts. The errors in V_ℓ are probably the weakest link in the calculation of all subsequent quantities.

The ohmic input power is simply calculated from

$$P_{OH} = I_P V_\ell \quad (8)$$

In addition to the errors in V_ℓ previously discussed, the ohmic input power is subject to assumptions about the plasma current profile, namely that the underestimate of P_{OH} for current flowing near the hoops where V_ℓ is small is just compensated by the overestimate of P_{OH} for current flowing near the wall where V_ℓ is large.

The electron temperature (in eV) is calculated from I_P and V_ℓ assuming Spitzer resistivity with $Z_{eff}=1$ and assuming the current is distributed uniformly over a circular cross-section of radius a :

$$T_e = 376(|I_P/V_\ell|/a^2)^{2/3} \quad (9)$$

The actual peak electron temperature is probably larger by a factor of $\sim 2-3$ because Z_{eff} is greater than 1 and the current is presumably somewhat peaked near the axis.

The average electron density is determined from the ion saturation current density J_{SAT} and the conductivity electron temperature using the usual Langmuir probe relation $J_{SAT} \propto n\sqrt{T_e}$ for $T_e > T_i$. However, the coefficient was adjusted so that the density determined in this fashion

agrees with the line-averaged density (averaged along the entire path between the interferometer horns) using a 72 GHz microwave interferometer for a standard discharge:

$$\langle n \rangle = \frac{0.05 J_{\text{SAT}}}{\sqrt{T_e} (1 - e^{-45/T_e})} \quad (10)$$

J_{SAT} is in mA/cm² and $\langle n \rangle$ is in 10¹² cm⁻³. The factor $1 - e^{-45/T_e}$ is included to account for the fact that only 45 V bias is used on the probe, and thus not all electrons are repelled when the temperature is high. This voltage is provided by a power supply but should be checked occasionally. The actual peak density depends on the profile and is probably ~2-3 times the value indicated here. The Langmuir probe is located on the octupole separatrix in the lower outer bridge and uses as a reference a large electrode which extends across the plasma nearly to the hoop in the upper outer bridge at the same (330 degree) toroidal azimuth.

Finally, the electron energy confinement time is calculated from

$$\tau = \frac{0.144 \langle n \rangle T_e}{P_{\text{OH}}} \quad (11)$$

where τ is in msec and the other units are as before (10¹² cm⁻³, eV, and kW). This confinement time assumes a quasi-steady state, i.e.: τ is much less than the time scale for change in either plasma energy or ohmic input power. In the above formula, the total machine volume inside ψ_{crit} is used (5×10⁵ cm³), and thus it represents an overall machine confinement time rather than a confinement time for the central current channel. As such, it

is probably an overestimate since the volume-averaged T_e is probably less than that calculated from the conductivity which assumes the current flows only within a radius a , unless Z_{eff} is high enough to compensate for this effect. To get an estimate of the confinement of the central current channel, one should use a smaller volume ($\sim 1 \times 10^5 \text{ cm}^{-3}$). However, since $\langle n \rangle T_e$ is low by a factor of $\sim 4-9$, the errors offset, and the calculated τ is probably a reasonable estimate for the confinement of the central current channel to within about a factor of two. It is interesting to note as pointed out by Prager that the method used to calculate τ involves multiplying the measured density by $I_H^{1/3} I_P^{-2/3} V_\ell^{-5/3}$, and thus the confinement time is most sensitive to the loop voltage and very little else. This is unfortunate since the error in V_ℓ exceeds that of any other quantity.

A-to-D Converter

The A-to-D converter is a Model AIM16, available for about \$300 from Connecticut Microcomputer, Inc., 150 Pocono Road, Brookfield, CT 06804. Excerpts from the Data Sheet are included in Appendix C. It has the virtue of being the first such unit made for the TRS-80 with specifications adequate for the present purpose. Better units are now available but at higher cost. The unit has 16 multiplexed inputs with a maximum conversion time of 100 μsec per channel. Each channel has 8-bit accuracy (0-255) and responds to positive voltages in the range 0-5.12 volts (20 mV resolution). The absolute maximum error is 10 mV + 0.7%. In order to achieve reasonable time resolution (500 μsec), only channels 1-5 are used for the high speed recording of data. The remaining channels are available for monitoring other slowly varying quantities, but only channel 6 is being used at present (to monitor neutral pressure). The unit has two significant limitations: 1) It does not have a sample-and-hold circuit and thus will

produce erroneous results if the input voltage varies significantly over the 100 μ sec conversion interval. 2) Saturation of any channel in either direction ($V_{in} < 0$ or > 5.12 volts) will produce erroneous readings in all the other channels during the time the channel is saturated.

The A-to-D converter was repackaged in a shielded rack panel with a filtered internal power supply (+5.12 volts), BNC input connectors, and 1 M Ω potentiometer gain adjustments on each channel. In addition, input filtering was provided to protect the AIM16 from noise, damage due to overvoltage, and rapidly changing input signals. The filtering typically limits the input response time to $> 24 \mu$ sec (< 6.6 kHz) on most channels. The input resistance of each channel is 1 M Ω , and a 10 k Ω input resistor protects the A-to-D from damage by overvoltage for any reasonable input signal. Some channels are provided with a dc offset to allow a negative voltage swing at the input. Although channel ϕ is designated as a trigger channel, the software actually uses channel 4 (V_{PG}). The trigger channel can be changed by POKEing an integer corresponding to the desired channel number (0-15) into memory location 32011 after the program is running (BASIC version only). A schematic of the input circuitry for the A-to-D converter is included in Appendix D.

Current Monitor Circuit

The A-to-D circuit requires inputs proportional to plasma current and hoop current to operate properly. Unfortunately, there is no simple, non-perturbing method for generating such signals. Rather, one has to take the available signals (poloidal gap voltage V_{PG} and primary current I_{PR} in the iron core) and deduce the plasma and hoop currents based upon some reasonable model of the plasma current profile. Several PLP's have been written on this subject (712, 756, 777), and the emphasis here will

therefore be on the circuitry used to generate the signals rather than the justification of the model. Simply stated, the model assumes that the plasma current profile is such that in some appropriate flux space average, the current can be treated as if it were all concentrated at the geometric axis (or octupole null). Then the circuit model of PLP 777 gives

$$I_P = \frac{N}{\alpha} I_{PR} - \frac{1}{\alpha L_H} \int V_{PG} dt + \frac{1}{\alpha L_H} \int I_H R_H dt \quad (12)$$

and

$$I_H = N I_{PR} - I_P \quad (13)$$

where N is the poloidal field turns ratio (typically 40). An analog computer circuit was constructed to calculate I_P and I_H . The circuit as shown in Appendix E uses 10 type 741 operational amplifiers and generates a number of other useful quantities:

$$\begin{aligned} \Phi &= \int V_{PG} dt && \text{(poloidal flux: 0.1 webers/volt)} \\ AS &= \int I_P dt && \text{(amp-seconds: 1000/volt)} \\ \dot{I}_P &= dI_P/dt && \text{(time derivative of } I_P \text{: 10 kA/msec/volt)} \end{aligned}$$

Actually, for calculating plasma current, the circuit solves the equation:

$$\begin{aligned} I_P &= AV_{PG} + BI_{PR} - 9.1 \int V_{PG} dt + C \int I_H dt \\ &\quad - D \int \left[\int I_{PR} dt \right] dt \end{aligned} \quad (14)$$

in which A, B, C, and D are constants adjustable from the front panel and labeled "EARLY", "MID", "LATE", and "VERY LATE" respectively. The first term (A) is typically small and corrects for stray capacitance not included

in the circuit model. The last term (D) compensates for magnetic field soak-in (\dot{R}_H , $\dot{\alpha}$, and \dot{L}_H) as well as the magnetizing inductance of the iron core and other effects which become important only after a long time. Note that one of the coefficients (9.1) is fixed by the circuit (corresponding to an initial hoop inductance of $L_H=0.22 \mu\text{H}$ and $\alpha=0.5$), such that the calibration of the plasma current is ensured once the other coefficients are adjusted to give $I_p=0$ at all times in the absence of a plasma. In practice, one adjusts the circuit so as to give as nearly a flat baseline as possible when the fields are pulsed in the absence of a plasma. The plasma current is filtered by an active RC low pass filter with a cutoff frequency of 1.6 kHz (100 μsec response time) to reduce high frequency noise. The circuit has only two inputs, V_{PG} and I_{PR} . These inputs enter the circuit through LC low-pass filters with a cutoff frequency of 160 kHz. The poloidal gap voltage is measured by a single loop of wire around the iron core. The primary current is determined by measuring the voltage across a $10^{-3} \Omega$ resistor (1 kA/volt) in series with the primary through a special, low-frequency, 1:2 turns ratio isolation transformer (Jensen Model JE-11S-L) to eliminate ground loops. The transformer is terminated in 150Ω through a 1 MH inductor to compensate for the inductance of the current shunt, to produce a 2:1 voltage reduction, and to increase the volt-second limit of the transformer. All grounds are referenced to the panel of the current monitor circuit, and the computer gets its ground through the signal cables that connect to the A-to-D converter. The computer rack should float if these cables are disconnected.

In order to account for the time-varying hoop resistance, a modification was made to the circuit in Appendix E using the results of a calculation by Kerst of the voltage at the surface of a Tokapole hoop versus

time in the presence of a current step. The actual current waveform can be decomposed into an infinite sum of such current steps. The calculation treats the hoop as a uniform cylinder with a constant poloidal field at its surface. The result is a time varying resistance given by

$$R_H(t) = R(o) \left[1 + \sum_{i=1}^{\infty} e^{-t/\tau_i} \right] \quad (15)$$

where in cgs units

$$\tau_i \cong \frac{4r_o^2}{\pi(i+0.24)^2 10^9 \rho} \quad (16)$$

In Eq. (16), r_o is the radius (2.5 cm) and ρ is the resistivity (2.2 $\mu\Omega$ -cm) of the hoops. The first 20 values of τ_i are tabulated in Appendix F along with a schematic of an RC network whose reciprocal (I/V) approximates this function and replaces the 100 k Ω resistor between the output of op amp 7 and the input of op amp 5 in Appendix E. Actually, the ratio of voltage to current is not purely resistive in either the hoops or in the circuit model since part of the voltage at the hoop surface is due to the time varying magnetic flux inside the hoops. In other words, the product of voltage and current does not give the instantaneous ohmic power dissipated by the hoops as was the case in Spencer's calculation (PLP 771). Thus the time dependent hoop resistance automatically accounts for that portion of the variation of the hoop inductance, $L_H(t)$, that is due to flux soaking into the hoops. When the current monitor circuit was modified in this way, the result was a considerably flatter baseline and a plasma current trace whose initial peak is suppressed and moved considerably later in time.

APPENDICES

- A. BASIC Listing of Tokapole Monitor Program
- B. AIM16 Machine Language Routine
- C. AIM16 Data Sheet Excerpts
- D. Schematic of A-to-D Input Circuit
- E. Schematic of Tokapole Current Monitor Circuit
- F. Schematic of Circuit to Model Hoop Resistance

APPENDIX A

BASIC Listing of Tokapole Monitor Program

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10 POKE16561,254:POKE16562,124:CLR:RESTORE:CLS:PRINTTAB(11)"TO
KAPOLE MONITOR PROGRAM / JCS / 26 JAN 83":CLEAR600:DEFINTA-R,T-Z
:DIMX(5,40),XB(5,40),GR(40),AS(127),S(13,10):M=MEM
20 IFM<>6769PRINT"MEMORY CHECK ERROR ON LOAD":PRINT"MEM ="M;"(S
HOULD BE 6769)":PRINT"TRY RELOADING CASSETTE":ENDELSEPOKE16526,1
:POKE16527,125:FORI=32001TO32145:READX:POKEI,X:NEXT
30 DATA62,1,50,44,126,62,192,211,223,62,4,211,223,58,1,56,33,2,5
6,182,33,4,56,182,33,16,56,182,33,64,56,182,192,62,255,211,223,2
19,223,203,127,40,222,14,206,33,45,126,22,1,122,211,223,20
40 DATA122,254,6,32,2,22,1,6,6,16,254,62,255,211,223,219,223,119
,122,211,223,35,13,32,230,62,0,50,44,126,42,42,126,1,45,126,30,4
1,22,5,54,0,35,54,0,35,10,119,35,54,0,3,21,32,246,35,29,32
50 DATA235,221,42,42,126,253,42,40,126,14,246,6,2,175,221,126,0,
253,158,0,221,119,0,221,35,253,35,16,241,13,32,235,201:PP=223:OU
TTP,128:FORI=1TO5:OUTPP,I:OUTPP,192:XB(I,0)=INP(PP):FORJ=1TO40:X
B(I,J)=XB(I,0):NEXTJ,I:FS=10:PRINT
60 SC(1)=1:SC(2)=10:SC(3)=200:SC(4)=0.5:SC(5)=2
70 IFBM=0PRINT"***** TAKE A BASELINE SHOT":
80 SET(125,0):OUTPP,128:OUTPP,6:OUTPP,192:PB=INP(PP):POKE32299,I
NT(VARPTR(X(0,0))/256):POKE32298,VARPTR(X(0,0))-256*INT(VARPTR(X
(0,0))/256):POKE32297,INT(VARPTR(XB(0,0))/256):POKE32296,VARPTR(
XB(0,0))-256*INT(VARPTR(XB(0,0))/256):X=USR(0)
90 OUTPP,128:OUTPP,6:OUTPP,192:PR=INP(PP):SET(127,0):IFPEEK(3230
0)THEN270ELSEBL=X(2,5)+X(2,10)+X(2,15):IFBL>5THENBL=1:GOTO110ELS
EBL=0:BM=1:FORI=1TO2:FORJ=0TO40:XB(I,J)=XB(I,J)+X(I,J):NEXT:NEXT
:FORI=3TO5:OUTPP,I:OUTPP,192:XB(I,0)=INP(PP)
100 FORJ=1TO40:XB(I,J)=XB(I,0):NEXT:NEXT
110 QI=0:IFBL>0THENNS=NS+1
120 CLS:IFBL=0THENPRINT"BASELINE"ELSEPRINT"SHOT NUMBER:"NS:IFAB
S(X(1,40))>9THENBM=0
130 IFABS(X(1,40))>1THENIH=0:FORJ=0TO40:IH=IH+X(5,J):NEXT:IFIHTH
ENIT=0:FORJ=0TO40:IT=IT+X(5,J):X(1,J)=X(1,J)-X(1,40)*IT/IH:NEXT
140 IM=X(1,0):AS=0:FORJ=0TO40:AS=AS+X(1,J):IFX(1,J)>=IMTHENIM=X(
1,J):JM=J
150 IFX(1,J)<0THENAS=AS-X(1,J)
160 NEXT
170 AS=AS*BM*BL:TM=5*JM+1:IFJM>0ANDJM<40THENS0=X(1,JM-1):S2=X(1,
JM+1):IF2*IM<>S0+S2THENTM=TM-2.5*(S2-S0)/(S2-2*IM+S0):IM=IM-0.10
0*(S2-S0)*(S2-S0)/(S2-2*IM+S0)
180 IFIMPRINT"MAX IP ="SC(1)*IM:"KA AT":TM/10:"MSEC"ELSEPRINT"M
AX IP = 0"
190 PRINT"AMP SECONDS ="SC(1)*AS/2:PRINT"PRES ="4*(PR-PB):"E-5
TORR":PRINT"TIME IP JSAT BT VPG IHOOB DIP
/DT":FORJ=1TO10:J1=FS*J/5:S(0,J)=FS*J/10:PRINTS(0,J):FORI=1TO5:
XP(I)=((5-I)*X(I,J1)+I*X(I,J1-1))/5
200 X1=BL*X(I,J1)+XB(I,J1):X2=BL*X(I,J1-1)+XB(I,J1-1):IFX1<=0ORX
2<=0PRINTTAB(8*I):"SAT-":GOTO210ELSEIFX1>=255ORX2>=255PRINTTAB(
8*I):"SAT+":GOTO210ELSE(I,J)=SC(I)*XP(I):PRINTTAB(8*I):S(I,J):
```

BASIC Listing of Teleside Test Program

```
10 PRINT "TELETYPE TEST PROGRAM"
20 INPUT "ENTER PROGRAM NAME: "; A$
30 IF A$="" THEN GOTO 40
40 PRINT "PROGRAM NAME: "; A$
50 INPUT "ENTER TEST NUMBER: "; B$
60 IF B$="" THEN GOTO 70
70 PRINT "TEST NUMBER: "; B$
80 GOTO 90
90 PRINT "TESTING PROGRAM: "; A$
100 PRINT "TEST NUMBER: "; B$
110 PRINT "TESTING PROGRAM: "; A$
120 PRINT "TEST NUMBER: "; B$
130 PRINT "TESTING PROGRAM: "; A$
140 PRINT "TEST NUMBER: "; B$
150 PRINT "TESTING PROGRAM: "; A$
160 PRINT "TEST NUMBER: "; B$
170 PRINT "TESTING PROGRAM: "; A$
180 PRINT "TEST NUMBER: "; B$
190 PRINT "TESTING PROGRAM: "; A$
200 PRINT "TEST NUMBER: "; B$
210 PRINT "TESTING PROGRAM: "; A$
220 PRINT "TEST NUMBER: "; B$
230 PRINT "TESTING PROGRAM: "; A$
240 PRINT "TEST NUMBER: "; B$
250 PRINT "TESTING PROGRAM: "; A$
260 PRINT "TEST NUMBER: "; B$
270 PRINT "TESTING PROGRAM: "; A$
280 PRINT "TEST NUMBER: "; B$
290 PRINT "TESTING PROGRAM: "; A$
300 PRINT "TEST NUMBER: "; B$
310 PRINT "TESTING PROGRAM: "; A$
320 PRINT "TEST NUMBER: "; B$
330 PRINT "TESTING PROGRAM: "; A$
340 PRINT "TEST NUMBER: "; B$
350 PRINT "TESTING PROGRAM: "; A$
360 PRINT "TEST NUMBER: "; B$
370 PRINT "TESTING PROGRAM: "; A$
380 PRINT "TEST NUMBER: "; B$
390 PRINT "TESTING PROGRAM: "; A$
400 PRINT "TEST NUMBER: "; B$
410 PRINT "TESTING PROGRAM: "; A$
420 PRINT "TEST NUMBER: "; B$
430 PRINT "TESTING PROGRAM: "; A$
440 PRINT "TEST NUMBER: "; B$
450 PRINT "TESTING PROGRAM: "; A$
460 PRINT "TEST NUMBER: "; B$
470 PRINT "TESTING PROGRAM: "; A$
480 PRINT "TEST NUMBER: "; B$
490 PRINT "TESTING PROGRAM: "; A$
500 PRINT "TEST NUMBER: "; B$
510 PRINT "TESTING PROGRAM: "; A$
520 PRINT "TEST NUMBER: "; B$
530 PRINT "TESTING PROGRAM: "; A$
540 PRINT "TEST NUMBER: "; B$
550 PRINT "TESTING PROGRAM: "; A$
560 PRINT "TEST NUMBER: "; B$
570 PRINT "TESTING PROGRAM: "; A$
580 PRINT "TEST NUMBER: "; B$
590 PRINT "TESTING PROGRAM: "; A$
600 PRINT "TEST NUMBER: "; B$
610 PRINT "TESTING PROGRAM: "; A$
620 PRINT "TEST NUMBER: "; B$
630 PRINT "TESTING PROGRAM: "; A$
640 PRINT "TEST NUMBER: "; B$
650 PRINT "TESTING PROGRAM: "; A$
660 PRINT "TEST NUMBER: "; B$
670 PRINT "TESTING PROGRAM: "; A$
680 PRINT "TEST NUMBER: "; B$
690 PRINT "TESTING PROGRAM: "; A$
700 PRINT "TEST NUMBER: "; B$
710 PRINT "TESTING PROGRAM: "; A$
720 PRINT "TEST NUMBER: "; B$
730 PRINT "TESTING PROGRAM: "; A$
740 PRINT "TEST NUMBER: "; B$
750 PRINT "TESTING PROGRAM: "; A$
760 PRINT "TEST NUMBER: "; B$
770 PRINT "TESTING PROGRAM: "; A$
780 PRINT "TEST NUMBER: "; B$
790 PRINT "TESTING PROGRAM: "; A$
800 PRINT "TEST NUMBER: "; B$
810 PRINT "TESTING PROGRAM: "; A$
820 PRINT "TEST NUMBER: "; B$
830 PRINT "TESTING PROGRAM: "; A$
840 PRINT "TEST NUMBER: "; B$
850 PRINT "TESTING PROGRAM: "; A$
860 PRINT "TEST NUMBER: "; B$
870 PRINT "TESTING PROGRAM: "; A$
880 PRINT "TEST NUMBER: "; B$
890 PRINT "TESTING PROGRAM: "; A$
900 PRINT "TEST NUMBER: "; B$
910 PRINT "TESTING PROGRAM: "; A$
920 PRINT "TEST NUMBER: "; B$
930 PRINT "TESTING PROGRAM: "; A$
940 PRINT "TEST NUMBER: "; B$
950 PRINT "TESTING PROGRAM: "; A$
960 PRINT "TEST NUMBER: "; B$
970 PRINT "TESTING PROGRAM: "; A$
980 PRINT "TEST NUMBER: "; B$
990 PRINT "TESTING PROGRAM: "; A$
1000 PRINT "TEST NUMBER: "; B$
```

```
210 NEXT J2=J1+1:IF J2=41 THEN J2=40
220 J0=J1-2:IF J0<0 THEN J0=0
230 S(13,J)=SC(1)*(8*X(1,J2)+2*X(1,J1)-8*X(1,J1-1)-2*X(1,J0))/10
:PRINT TAB(48)S(13,J):NEXT:IF BL=0 THEN 260 ELSE NT=127:IF NS<128 THEN NT
=NS
240 IF NS>127 FOR I=1 TO 127:AS(I-1)=AS(I):NEXT
250 AS(NT)=AS
260 IF CS<>" THEN GOSUB 530:IF QQ<>" THEN 280
270 QQ=INKEY$:IF QQ="" THEN 70
280 IF QQ="0" THEN PRINT "***** COMPUTER ON STANDBY---PRESS 1 TO C
ONTINUE TAKING DATA";
290 IF QQ="0" THEN IF INKEY$<>"1" THEN 290 ELSE CLS:GOTO 70 ELSE IF QQ="1"
THEN 70 ELSE CLS:PRINT AS/2;"AS";:IF QQ="I" THEN PRINT,"PLASMA CURRENT
VS TIME";:IG=1:GOTO 350 ELSE IF QQ="J" THEN PRINT,"ION SATURATION CU
RRENT VS TIME";:IG=2:GOTO 350
300 IF QQ="B" THEN PRINT,"TOROIDAL FIELD VS TIME";:IG=3:GOTO 350 ELSE
IF QQ="V" THEN PRINT,"POLOIDAL GAP VOLTAGE VS TIME";:IG=4:GOTO 350
ELSE IF QQ="H" THEN PRINT,"HOOP CURRENT VS TIME";:IG=5:GOTO 350 ELSE
IF QQ="C" THEN CLS:GOSUB 400:GOTO 120 ELSE IF QQ="R" THEN 120
310 IF QQ="S" THEN CLS:PRINT "CURRENT SHOT NUMBER =";NS:INPUT "NEW S
HOT NUMBER";NS:GOTO 70 ELSE IF QQ="L" THEN GOSUB 410:GOTO 260 ELSE IF QQ=
"E" THEN GOSUB 430:GOTO 280 ELSE IF QQ="A" THEN GOSUB 450:GOTO 260 ELSE IF QQ
="M" THEN GOSUB 550:GOTO 280 ELSE CLS:PRINT "COMMANDS:";
320 PRINT,"0: STANDBY":PRINT,"1: CONTINUE":PRINT,"I: GRAPH PLASM
A CURRENT":PRINT,"J: GRAPH ION SATURATION CURRENT":PRINT,"B: GRA
PH TOROIDAL FIELD":PRINT,"V: GRAPH POLOIDAL GAP VOLTAGE":PRINT,"
H: GRAPH HOOP CURRENT":PRINT,"C: CHANGE TIME SCALE"
330 PRINT,"L: GRAPH A-S FOR LAST";NT;"SHOTS":PRINT,"R: RETURN TO
INITIAL TABLE":PRINT,"S: CHANGE SHOT NUMBER COUNTER":PRINT,"E:
EXAMINE ANALOG INPUTS":PRINT,"A: DISPLAY DERIVED DATA":PRINT,"M:
PRINT MESSAGE ON SCREEN"
340 PRINT,"P: PROGRAM COMMAND SEQUENCE":IF QQ="P" THEN CS="" :INPU
T "WHAT COMMAND SEQUENCE";CS:GOTO 70 ELSE 260
350 IF BL=1 PRINT TAB(52);"SHOT";NS:ELSE PRINT TAB(52);"BASELINE";
360 Y1=0:Y2=0:FOR J=0 TO 40:GR(J)=X(IG,J):IF GR(J)>Y2 THEN Y2=GR(J)
370 IF GR(J)<Y1 THEN Y1=GR(J)
380 NEXT:IF Y2=Y1 PRINT:PRINT:PRINT "***** NO DATA TO GRAPH":GOTO 2
60 ELSE SY=34/(Y2-Y1):FOR J=0 TO 40:SET(3*J+5,44.5-SY*(GR(J)-Y1)):NEX
T:Y=44.5+SY*Y1:FOR I=3 TO 125:SET(I,Y):NEXT:FOR Y=15553 TO 16257 STEP 64
:POKEY,170:NEXT
390 PRINT@961,"0      2      4      6      8      MSEC  12      14      1
6      18      20";:PRINT@80,"MAXIMUM VALUE:";SC(IG)*Y2;:GOTO 260
400 FS=10:INPUT "HOW MANY MSEC FULL SCALE (DEFAULTS TO 10)";FS:IF
FS>20 PRINT "MAXIMUM IS 20 MSEC":GOTO 400 ELSE IF FS<5 PRINT "MINIMUM IS
5 MSEC":GOTO 400 ELSE CLS:RETURN
```

```
230 PRINT "MAXIMUM IS 20 NSEC";GOTO400ELSERPRINT"MINIMUM IS
240 PRINT"HOW MANY NSEC FULL SCALE (DEFAULTS TO 10)";GOTO400
250 PRINT80,"MAXIMUM VALUE";GOTO400
260 PRINT100,"MSEC";GOTO400
270 GOTO400
280 NEXT I;Y;Z;PRINT"***** NO DATA TO GRAPH";GOTO3
290 GOTO400
300 GOTO400
310 GOTO400
320 GOTO400
330 GOTO400
340 GOTO400
350 GOTO400
360 GOTO400
370 GOTO400
380 GOTO400
390 GOTO400
400 GOTO400
410 GOTO400
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930 GOTO400
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950 GOTO400
960 GOTO400
970 GOTO400
980 GOTO400
990 GOTO400
1000 GOTO400
```



```
410 PRINT,"AMP SECONDS FOR LAST";NT;"SHOTS":Y2=0:FORI=0TONT:IFAS
(I)>Y2THENY2=AS(I)
420 NEXT:IFY2=0PRINT:PRINT" **** NO DATA TO GRAPH":RETURNELSEPR
INT@960,STRING$(63,CHR$(176));:POKE16363,176:FORI=1TONT:SET(I,47
-41*AS(I)/Y2):NEXT:FORY=6T046:SET(0,Y):NEXT:PRINT@80,"MAXIMUM VA
LUE":Y2*SC(1)/2;:RETURN
430 CLS:PRINT,"ANALOG INPUT FOR EACH CHANNEL":PRINT:OUTPP,128:FO
RI=0T015:PRINTUSING"####";I;:NEXT:PRINT@396,"PRESS ANY KEY TO RE
SUME TOKAPOLE DATA"
440 PRINT@192,"";:FORI=0T015:OUTPP,I:OUTPP,192:PRINTUSING"####";
INP(PP);:NEXT:QQ$=INKEY$:IFQQ$=""THEN440ELSERETURN
450 PRINT,"ADDITIONAL DERIVED DATA";:IFBL=1PRINTTAB(52);"SHOT";N
SELSEPRINTTAB(52);"BASELINE"
460 PRINT:PRINT"TIME      A          <Q>      VLOOP    POH      TE
<N>      TAU":FORJ=1T010:IFS(5,J)THENS(6,J)=17.4*(ABS(S(1,J)/S(5,
J)))1.25ELSES(6,J)=0
470 IFS(1,J)THENS(7,J)=1E-4*S(6,J)*S(6,J)*S(3,J)/S(1,J)ELSES(7,J
)=0
480 S(8,J)=.5*(1+S(0,J)/75)*S(4,J)+.0045*(1-S(0,J)/37)*S(5,J):IF
S(6,J)THENS(8,J)=S(8,J)-2.3*S(13,J)/SQR(S(6,J))
490 S(9,J)=S(8,J)*S(1,J):IFS(8,J)*S(6,J)THENS(10,J)=376*(ABS(S(1
,J)/S(8,J)/S(6,J)/S(6,J)))1.6666667ELSES(10,J)=0
500 IFS(10,J)>0THENS(11,J)=.050*S(2,J)/SQR(S(10,J))/(1-EXP(-45/S
(10,J)))ELSES(11,J)=0
510 IFS(9,J)THENS(12,J)=.144*S(11,J)*S(10,J)/S(9,J)ELSES(12,J)=0
520 PRINTTAB(0)S(0,J);:FORI=6T012:PRINTTAB(8*I-41)INT(100*S(I,J)
+.5)/100;:NEXT:PRINT:NEXT:PRINT"MSEC      CM          VOLTS
KW      EV      E12/CC  MSEC":RETURN
530 LS=LEN(CS$):QI=QI+1:IFQI<=LSTHENQQ$=MID$(CS$,QI,1)ELSEQQ$=""
540 FORI=0T0600*VAL(QQ$):NEXT:IFVAL(QQ$)THEN530ELSERETURN
550 CLS:INPUT"MESSAGE";M$:CLS:IFLEN(M$)<192THENMM$=STRING$(31,"
")+M$ELSEMM$=M$
560 FORI=1T0LEN(MM$):PRINT@448,CHR$(23);MID$(MM$,I,31);STRING$(3
1," "):FORJ=1T050:NEXTJ,I:QQ$=INKEY$:IFQQ$=""THEN560ELSECLS:RETU
RN
```



```
10 POKF14541,252:POKF14542,118:CLEAF:RESTORE:CLS:PRINTTAB(11)"TO
KAPOLF MONITOR PROGRAM / JCS / 28 JAN 83":CLEAF600:DEFINTA-R,T-Z
:DTM(5,40),YB(5,40),GP(40),AS(127),S(13,10)
20 PRINTTAB(24)"COMPILED VERSION":POKE16526,1:POKE16527,125:FORI
=32001TO32145:PEADY:POKEI,X:NEXT
30 DATA62,1,50,44,126,62,192,211,223,62,4,211,223,58,1,56,33,2,5
6,182,33,4,56,182,33,16,56,182,33,64,56,182,192,62,255,211,223,2
19,223,203,127,40,222,14,206,33,45,126,22,1,122,211,223,20
40 DATA122,254,6,32,2,22,1,6,6,16,254,62,255,211,223,219,223,119
,122,211,223,35,13,32,230,62,0,50,44,126,42,42,126,1,45,126,30,4
1,22,5,54,0,35,54,0,35,10,119,35,54,0,3,21,32,246,35,29,32
50 DATA35,221,42,42,126,253,42,40,126,14,246,6,2,175,221,126,0,
253,158,0,221,119,0,221,35,253,35,16,241,13,32,235,201:PP=223:OU
TTP,128:FORI=1TO5:OUTPP,I:OUTPP,192:XB(I,0)=INP(PP):FORJ=1TO40:X
B(I,J)=YB(I,0):NEXTJ,I:FS=10:PRINT
60 SC(1)=1:SC(2)=10:SC(3)=200:SC(4)=0,5:SC(5)=2
70 IFBM=0PRINT"***** TAKE A BASELINE SHOT";
80 SET(125,0):OUTPP,128:OUTPP,6:OUTPP,192:PB=INP(PP):POKE32299,I
NT(VARPTR(X(0,0))/256):POKE32298,VARPTR(X(0,0))-256*INT(VARPTR(X
(0,0))/256):POKE32297,INT(VARPTR(XB(0,0))/256):POKE32296,VARPTR(
XB(0,0))-256*INT(VARPTR(XB(0,0))/256):X=USR(0)
90 OUTPP,128:OUTPP,6:OUTPP,192:PR=INP(PP):SET(127,0):IFPEEK(3230
0)THEN270ELSEBL=X(2,5)+X(2,10)+X(2,15):IFBL>5THENBL=1:GOTO110ELS
EBL=0:BM=1:FORI=1TO2:FORJ=0TO40:XB(I,J)=XB(I,J)+X(I,J):NEXT:NEXT
:FORI=3TO5:OUTPP,I:OUTPP,192:XB(I,0)=INP(PP)
100 FORJ=1TO40:XB(I,J)=XB(I,0):NEXT:NEXT
110 QI=0:IFBL>0THENNS=NS+1
120 CLS:IFBL=0THENPRINT"BASELINE"ELSEPRINT"SHOT NUMBER:";NS:IFAB
S(X(1,40))>9THENEM=0
130 IFABS(X(1,40))>1THENIH=0:FORJ=0TO40:IH=IH+X(5,J):NEXT:IFIHTH
ENIT=0:FORJ=0TO40:IT=IT+X(5,J):X(1,J)=X(1,J)-X(1,40)*IT/IH:NEXT
140 IM=X(1,0):AS=0:FORJ=0TO40:AS=AS+X(1,J):IFX(1,J)>=IMTHENIM=X(
1,J):JM=J
150 IFX(1,J)<0THENAS=AS-X(1,J)
160 NEXT
170 AS=AS*BM*BL:TM=5*JM+1:IFJM>0ANDJM<40THENS0=X(1,JM-1):S2=X(1,
JM+1):IF2*IM<>S0+S2THENTM=TM-2,5*(S2-S0)/(S2-2*IM+S0):IM=IM-0,10
0*(S2-S0)*(S2-S0)/(S2-2*IM+S0)
180 IFIMPRINT"MAX IP =" ;SC(1)*IM;"KA AT";TM/10;"MSEC"ELSEPRINT"M
AX IP = 0"
190 PRINT"AMP SECONDS =" ;SC(1)*AS/2:PRINT"PRES =" ;4*(PR-PB);"E-5
TORR":PRINT"TIME IP JSAT BT VPG IHOOP DIP
/DT":FORJ=1TO10:J1=FS*J/5:S(0,J)=FS*J/10:PRINTS(0,J);:FORI=1TO5:
XP(I)=((5-I)*X(I,J1)+I*X(I,J1-1))/5
200 X1=BL*X(I,J1)+XB(I,J1):X2=BL*X(I,J1-1)+XB(I,J1-1):IFX1<=0ORX
2<=0PRINTTAB(8*I);"SAT-";:GOTO210ELSEIFX1>=255ORX2>=255PRINTTAB(
8*I);"SAT+";:GOTO210ELSE(S(I,J)=SC(I)*XP(I):PRINTTAB(8*I);S(I,J);
```



```
210 NEXT J2=J1+1:IF J2=41 THEN J2=40
220 J0=J1-2:IF J0<0 THEN J0=0
230 S(13,J)=SC(1)*(8*X(1,J2)+2*X(1,J1)-8*X(1,J1-1)-2*X(1,J0))/10
:PRINT TAB(48)S(13,J):NEXT:IF BFL=0 THEN 260 ELSE NT=127:IF NS<128 THEN NT
=NS
240 IF NS>127 FOR I=1 TO 127:AS(I-1)=AS(I):NEXT
250 AS(NT)=AS
260 IFCS<>" " THEN GOSUB 530:IF QQ<>" " THEN 280
270 QQ=INKEY$:IF QQ="" THEN 70
280 IF QQ="" THEN PRINT " ***** COMPUTER ON STANDBY---PRESS 1 TO C
ONTINUE TAKING DATA";
290 IF QQ="" THEN IF INKEY$<>"1" THEN 290 ELSE CLS:GOTO 70 ELSE IF QQ="1"
THEN 70 ELSE CLS:PRINT AS/2;"AS";:IF QQ="I" THEN PRINT,"PLASMA CURRENT
VS TIME";:IG=1:GOTO 350 ELSE IF QQ="J" THEN PRINT,"ION SATURATION CU
RRENT VS TIME";:IG=2:GOTO 350
300 IF QQ="B" THEN PRINT,"TOROIDAL FIELD VS TIME";:IG=3:GOTO 350 EL
S IF QQ="V" THEN PRINT,"POLOIDAL GAP VOLTAGE VS TIME";:IG=4:GOTO 350
ELSE IF QQ="H" THEN PRINT,"HOOP CURRENT VS TIME";:IG=5:GOTO 350 ELSE I
F QQ="C" THEN CLS:GOSUB 400:GOTO 120 ELSE IF QQ="R" THEN 120
310 IF QQ="S" THEN CLS:PRINT"CURRENT SHOT NUMBER =";NS:INPUT"NEW S
HOT NUMBER";NS:GOTO 70 ELSE IF QQ="L" THEN GOSUB 410:GOTO 260 ELSE IF QQ="
E" THEN GOSUB 430:GOTO 280 ELSE IF QQ="A" THEN GOSUB 450:GOTO 260 ELSE IF QQ
="M" THEN GOSUB 550:GOTO 280 ELSE CLS:PRINT"COMMANDS:";
320 PRINT,"0: STANDBY":PRINT,"1: CONTINUE":PRINT,"I: GRAPH PLASMA
CURRENT":PRINT,"J: GRAPH ION SATURATION CURRENT":PRINT,"B: GRA
PH TOROIDAL FIELD":PRINT,"V: GRAPH POLOIDAL GAP VOLTAGE":PRINT,"
H: GRAPH HOOP CURRENT":PRINT,"C: CHANGE TIME SCALE"
330 PRINT,"L: GRAPH A-S FOR LAST";NT;"SHOTS":PRINT,"R: RETURN TO
INITIAL TABLE":PRINT,"S: CHANGE SHOT NUMBER COUNTER":PRINT,"E:
EXAMINE ANALOG INPUTS":PRINT,"A: DISPLAY DERIVED DATA":PRINT,"M:
PRINT MESSAGE ON SCREEN"
340 PRINT,"P: PROGRAM COMMAND SEQUENCE":IF QQ="P" THEN CS="" :INPU
T"WHAT COMMAND SEQUENCE";CS:GOTO 70 ELSE 260
350 IF BFL=1 PRINT TAB(52);"SHOT";NS;ELSE PRINT TAB(52);"BASELINE";
360 Y1=0:Y2=0:FOR J=0 TO 40:GR(J)=X(IG,J):IF GR(J)>Y2 THEN Y2=GR(J)
370 IF GR(J)<Y1 THEN Y1=GR(J)
380 NEXT:IF Y2=Y1 PRINT:PRINT" ***** NO DATA TO GRAPH":GOTO 2
60 ELSE SY=34/(Y2-Y1):FOR J=0 TO 40:SET(3*J+5,44.5-SY*(GR(J)-Y1)):NEX
T:Y=44.5+SY*Y1:FOR I=3 TO 125:SET(I,Y):NEXT:FOR Y=15553 TO 16257 STEP 64
:POKEY,170:NEXT
390 PRINT@961,"0      2      4      6      8      MSEC      12      14      1
6      18      20";:PRINT@80,"MAXIMUM VALUE:";SC(IG)*Y2:GOTO 260
400 FS=10:INPUT"HOW MANY MSEC FULL SCALE (DEFAULTS TO 10)";FS:IF
FS>20 PRINT"MAXIMUM IS 20 MSEC":GOTO 400 ELSE IF FS<5 PRINT"MINIMUM IS
5 MSEC":GOTO 400 ELSE CLS:RETURN
```



```
410 PRINT,"AMP SECONDS FOR LAST";NT;"SHOTS";Y2=0;FORI=0TONT;IFAS
(I)>Y2THENY2=AS(I)
420 NEXT;IFY2=0PRINT;PRINT" **** NO DATA TO GRAPH";RETURNELSEPR
INT@960,STRING$(63,CHR$(176));;POKE16363,176;FORI=1TONT;SET(I,47
-41*AS(I)/Y2);NEXT;FORY=6T046;SET(0,Y);NEXT;PRINT@80,"MAXIMUM VA
LUE";Y2*SC(1)/2;;RETURN
430 CLS;PRINT,"ANALOG INPUT FOR EACH CHANNEL";PRINT;OUTPP,128;FO
RI=0T015;PRINTUSING"####";I;;NEXT;PRINT@396,"PRESS ANY KEY TO RE
SUME TOKAPOLE DATA"
440 PRINT@192,"";;FORI=0T015;OUTPP,I;OUTPP,192;PRINTUSING"####";
INP(PP);;NEXT;QQ$=INKEY$;IFQQ$=""THEN440ELSERETURN
450 PRINT,"ADDITIONAL DERIVED DATA";;IFBL=1PRINTTAB(52);"SHOT";N
ELSEPRINTTAB(52);"BASELINE"
460 PRINT;PRINT"TIME      A          <Q>      VLOOP   POH      TE
<N>      TAU";FORJ=1T010;IFS(5,J)THENS(6,J)=17.4*(ABS(S(1,J)/S(5,
J)))[.25ELSE(S(6,J)=0
470 IFS(1,J)THENS(7,J)=1E-4*S(6,J)*S(6,J)*S(3,J)/S(1,J)ELSE(S(7,J
)=0
480 S(8,J)=.5*(1+S(0,J)/75)*S(4,J)+.0045*(1-S(0,J)/37)*S(5,J);IF
S(6,J)THENS(8,J)=S(8,J)-2.3*S(13,J)/SQR(S(6,J))
490 S(9,J)=S(8,J)*S(1,J);IFS(8,J)*S(6,J)THENS(10,J)=376*(ABS(S(1
,J)/S(8,J)/S(6,J)/S(6,J)))[.66666667ELSE(S(10,J)=0
500 IFS(10,J)>0THENS(11,J)=.050*S(2,J)/SQR(S(10,J))/(1-EXP(-45/S
(10,J)))ELSE(S(11,J)=0
510 IFS(9,J)THENS(12,J)=.144*S(11,J)*S(10,J)/S(9,J)ELSE(S(12,J)=0
520 PRINTTAB(0)S(0,J);;FORI=6T012;PRINTTAB(8*I-41)INT(100*S(I,J)
+.5)/100;;NEXT;PRINT;NEXT;PRINT"MSEC      CM              VOLTS
KW      EV      E12/CC  MSEC";RETURN
530 LS=LEN(CS$);QI=QI+1;IFQI<=LSTHENQQ$=MID$(CS$,QI,1)ELSEQQ$=""
540 FORI=0T04200*VAL(QQ$);NEXT;IFVAL(QQ$)THEN530ELSERETURN
550 CLS;INPUT"MESSAGE";M$;CLS;IFLEN(M$)<192THENMM$=STRING$(31,"
")+M$ELSEMM$=M$
560 FORI=1TOLEN(MM$);PRINT@448,CHR$(23);MID$(MM$,I,31);STRING$(3
1," ");;FORJ=1T0350;NEXTJ,I;QQ$=INKEY$;IFQQ$=""THEN560ELSECLS;RET
URN
```


TOKAPOKE MONITOR -- AIM16 ROUTINE

APPENDIX B

AIM16 Machine Language Routine

7D01		00100	ORG	32001	
7D01	3E01	00110	LD	A,1	
7D03	322C7E	00120	LD	(32300),A;STORE 1 IN 32300	
	06 3EC0	00130	LD	A,192	
0D08	D3DF	00140	OUT	(223),A ;INITIALIZE SYSTEM	
7D0A	3E00	00150	NOSIG LD	A,0	
7D0C	D3DF	00160	OUT	(223),A ;SELECT TRIGGER CHANNEL	
7D0E	3A0138	00170	LD	A,(3801H);STROBE KEYBOARD	
7D11	210238	00180	LD	HL,3802H	
7D14	B6	00190	OR	(HL)	
7D15	210438	00200	LD	HL,3804H	
7D18	B6	00210	OR	(HL)	
7D19	211038	00220	LD	HL,3810H	
7D1C	B6	00230	OR	(HL)	
7D1D	214038	00240	LD	HL,3840H	
7D20	B6	00250	OR	(HL) ;SET FLAG IF KEY PRESSED	
7D21	C0	00260	RET	NZ ;RETURN IF KEY PRESSED	
7D22	3EFF	00270	LD	A,255	
7D24	D3DF	00280	OUT	(223),A ;ENABLE TRIGGER	
7D26	DEDF	00290	IN	A,(223) ;READ TRIGGER SIGNAL	
7D28	CB7F	00300	BIT	7,A ;TEST HIGH ORDER BIT	
7D2A	28DE	00310	JR	Z,NOSIG ;RETURN IF TRIGGER < 128	
7D2C	0ECE	00320	LD	C,206 ;NUMBER OF POINTS	
7D2E	212D7E	00330	LD	HL,32301;BEGINNING MEMORY ADDRESS	
7D31	1601	00340	LD	D,1	
7D33	7A	00350	LD	A,D	
7D34	D3DF	00360	OUT	(223),A ;SELECT CHANNEL 1	
7D36	14	00370	CONT INC	D ;INCREMENT CHANNEL NUMBER	
7D37	7A	00380	LD	A,D	
7D38	FE06	00390	CF	6 ;HIGHEST CHANNEL # EXCEEDED?	
7D3A	2002	00400	JR	NZ,MORE ;GOTO MORE IF D<>6	
7D3C	1601	00410	LD	D,1 ;RESET TO FIRST CHANNEL	
7D3E	0606	00420	MORE LD	B,6 ;DELAY BETWEEN POINTS	
7D40	10FE	00430	LOOP DJNZ	LOOP ;LOOP UNTIL B=0	
7D42	3EFF	00440	LD	A,255	
7D44	D3DF	00450	OUT	(223),A ;ENABLE DATA	
7D46	DEDF	00460	IN	A,(223) ;READ DATA	
7D48	77	00470	LD	(HL),A ;STORE DATA	
7D49	7A	00480	LD	A,D	
7D4A	D3DF	00490	OUT	(223),A ;SELECT CHANNEL	
7D4C	23	00500	INC	HL ;INCREMENT MEMORY LOCATION	
7D4D	0D	00510	DEC	C ;DECREASE C BY 1	
7D4E	20E6	00520	JR	NZ,CONT ;CONTINUE IF MORE DATA	
7D50	3E00	00530	LD	A,0	
7D52	322C7E	00540	LD	(32300),A;STORE 0 IN 32300	
7D55	2A2A7E	00550	LD	HL,(32298);X BLOCK ADDRESS	
7D58	012D7E	00560	LD	BC,32301;DATA BLOCK ADDRESS	
7D5B	1E29	00570	LD	E,41 ;# OF TIMES	
7D5D	1605	00580	JLOOP LD	D,5 ;# OF CHANNELS	
7D5F	3600	00590	LD	(HL),0	
7D61	23	00600	INC	HL	
7D62	3600	00610	LD	(HL),0	
7D64	23	00620	ILOOP INC	HL	
7D65	0A	00630	LD	A,(BC) ;MOVE DATA	
7D66	77	00640	LD	(HL),A	
7D67	23	00650	INC	HL	
7D68	3600	00660	LD	(HL),0	
7D6A	03	00670	INC	BC ;NEXT DATA POINT	
7D6B	15	00680	DEC	D	
7D6C	20F6	00690	JR	NZ,ILOOP;GOTO ILOOP IF D>0	
7D6E	23	00700	INC	HL	
7D6F	1D	00710	DEC	E	

Address	Operation	Comment
0000	HL	
0001	INC	
0002	INC	
0003	INC	
0004	INC	
0005	INC	
0006	INC	
0007	INC	
0008	INC	
0009	INC	
000A	INC	
000B	INC	
000C	INC	
000D	INC	
000E	INC	
000F	INC	
0010	INC	
0011	INC	
0012	INC	
0013	INC	
0014	INC	
0015	INC	
0016	INC	
0017	INC	
0018	INC	
0019	INC	
001A	INC	
001B	INC	
001C	INC	
001D	INC	
001E	INC	
001F	INC	
0020	INC	
0021	INC	
0022	INC	
0023	INC	
0024	INC	
0025	INC	
0026	INC	
0027	INC	
0028	INC	
0029	INC	
002A	INC	
002B	INC	
002C	INC	
002D	INC	
002E	INC	
002F	INC	
0030	INC	
0031	INC	
0032	INC	
0033	INC	
0034	INC	
0035	INC	
0036	INC	
0037	INC	
0038	INC	
0039	INC	
003A	INC	
003B	INC	
003C	INC	
003D	INC	
003E	INC	
003F	INC	
0040	INC	
0041	INC	
0042	INC	
0043	INC	
0044	INC	
0045	INC	
0046	INC	
0047	INC	
0048	INC	
0049	INC	
004A	INC	
004B	INC	
004C	INC	
004D	INC	
004E	INC	
004F	INC	
0050	INC	
0051	INC	
0052	INC	
0053	INC	
0054	INC	
0055	INC	
0056	INC	
0057	INC	
0058	INC	
0059	INC	
005A	INC	
005B	INC	
005C	INC	
005D	INC	
005E	INC	
005F	INC	
0060	INC	
0061	INC	
0062	INC	
0063	INC	
0064	INC	
0065	INC	
0066	INC	
0067	INC	
0068	INC	
0069	INC	
006A	INC	
006B	INC	
006C	INC	
006D	INC	
006E	INC	
006F	INC	
0070	INC	
0071	INC	
0072	INC	
0073	INC	
0074	INC	
0075	INC	
0076	INC	
0077	INC	
0078	INC	
0079	INC	
007A	INC	
007B	INC	
007C	INC	
007D	INC	
007E	INC	
007F	INC	
0080	INC	
0081	INC	
0082	INC	
0083	INC	
0084	INC	
0085	INC	
0086	INC	
0087	INC	
0088	INC	
0089	INC	
008A	INC	
008B	INC	
008C	INC	
008D	INC	
008E	INC	
008F	INC	
0090	INC	
0091	INC	
0092	INC	
0093	INC	
0094	INC	
0095	INC	
0096	INC	
0097	INC	
0098	INC	
0099	INC	
009A	INC	
009B	INC	
009C	INC	
009D	INC	
009E	INC	
009F	INC	
00A0	INC	
00A1	INC	
00A2	INC	
00A3	INC	
00A4	INC	
00A5	INC	
00A6	INC	
00A7	INC	
00A8	INC	
00A9	INC	
00AA	INC	
00AB	INC	
00AC	INC	
00AD	INC	
00AE	INC	
00AF	INC	
00B0	INC	
00B1	INC	
00B2	INC	
00B3	INC	
00B4	INC	
00B5	INC	
00B6	INC	
00B7	INC	
00B8	INC	
00B9	INC	
00BA	INC	
00BB	INC	
00BC	INC	
00BD	INC	
00BE	INC	
00BF	INC	
00C0	INC	
00C1	INC	
00C2	INC	
00C3	INC	
00C4	INC	
00C5	INC	
00C6	INC	
00C7	INC	
00C8	INC	
00C9	INC	
00CA	INC	
00CB	INC	
00CC	INC	
00CD	INC	
00CE	INC	
00CF	INC	
00D0	INC	
00D1	INC	
00D2	INC	
00D3	INC	
00D4	INC	
00D5	INC	
00D6	INC	
00D7	INC	
00D8	INC	
00D9	INC	
00DA	INC	
00DB	INC	
00DC	INC	
00DD	INC	
00DE	INC	
00DF	INC	
00E0	INC	
00E1	INC	
00E2	INC	
00E3	INC	
00E4	INC	
00E5	INC	
00E6	INC	
00E7	INC	
00E8	INC	
00E9	INC	
00EA	INC	
00EB	INC	
00EC	INC	
00ED	INC	
00EE	INC	
00EF	INC	
00F0	INC	
00F1	INC	
00F2	INC	
00F3	INC	
00F4	INC	
00F5	INC	
00F6	INC	
00F7	INC	
00F8	INC	
00F9	INC	
00FA	INC	
00FB	INC	
00FC	INC	
00FD	INC	
00FE	INC	
00FF	INC	

7D70	20EB	00720	JR	NZ,JLOOP;GOTO JLOOP IF E>0
7D72	DD2A2A7E	00730	LD	IX,(32298);START X ADDRESS
7D76	FD2A287E	00740	LD	IY,(32296);START XB ADDRESS
7D7A	0EF6	00750	LD	C,246 ;# OF X VALUES
7D7C	0602	00760	LD	B,2 ;# OF BYTES/VALUE
7D7E	AF	00770	XOR	A ;RESET CARRY
7D7F	DD7E00	00780	LD	A,(IX) ;GET X
7D82	FD9E00	00790	SEC	A,(IY) ;SUBTRACT XB
7D85	DD7700	00800	LD	(IX),A ;STORE RESULT
7D88	DD23	00810	INC	IX ;PNT TO NEXT HIGHER X
7D8A	FD23	00820	INC	IY ;PNT TO NEXT HIGHER XB
7D8C	10F1	00830	DJNZ	BLOOP ;GOTO BLOOP IF MORE
7D8E	0D	00840	DEC	C ;NEXT VALUE
7D8F	20EB	00850	JR	NZ,BLINE;GOTO BLINE IF MORE
7D91	C9	00860	RET	
7D01		00870	END	32001
00000	TOTAL ERRORS			
BLOOP	7D7F			
BLINE	7D7C			
ILOOP	7D64			
JLOOP	7D5D			
LOOP	7D40			
MORE	7D3E			
CONT	7D36			
NOSIG	7D0A			

AIM16 Data Sheet Excerpts

AIM16 DATA SHEET

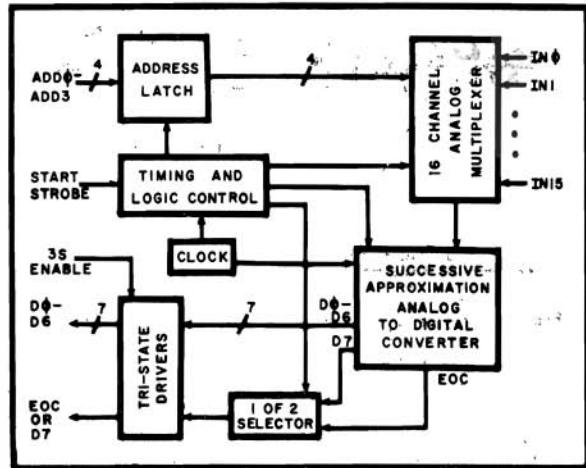
ANALOG PORT - 16 Channels - Specifications for each channel -
 V_{in} - analog input voltage conversion range: 0 to 5.12 volts
 V_{in} (max) - absolute maximum input voltage: -.3 to plus 5.4 volts
 I_{in} (max) - maximum analog input current: 2 microamps
 V_{ref} - reference voltage: 5.120 volts plus or minus .01 volts

Conversion data -

T_c - conversion time, per channel: 100 microsec max, 80 typ
 counts per channel: 256
 output range (each channel): 00-FF (hex)
 0-255 (decimal)
 000-377 (octal)
 0000 0000-1111 1111 (binary)

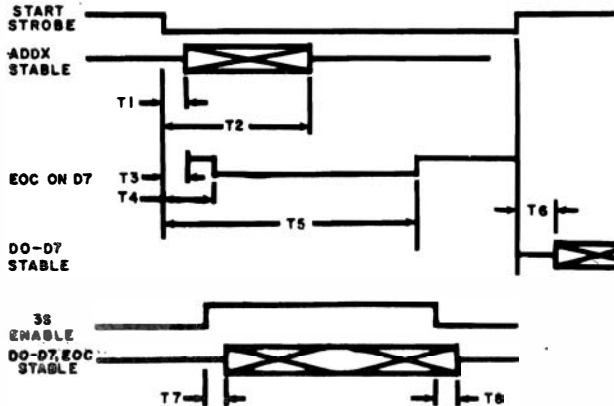
Absolute maximum error: .7%
 Typical maximum error: .5%

Physical Dimensions - 5 1/4 x 6 1/4 x 2 1/4.



AIM16 BLOCK DIAGRAM

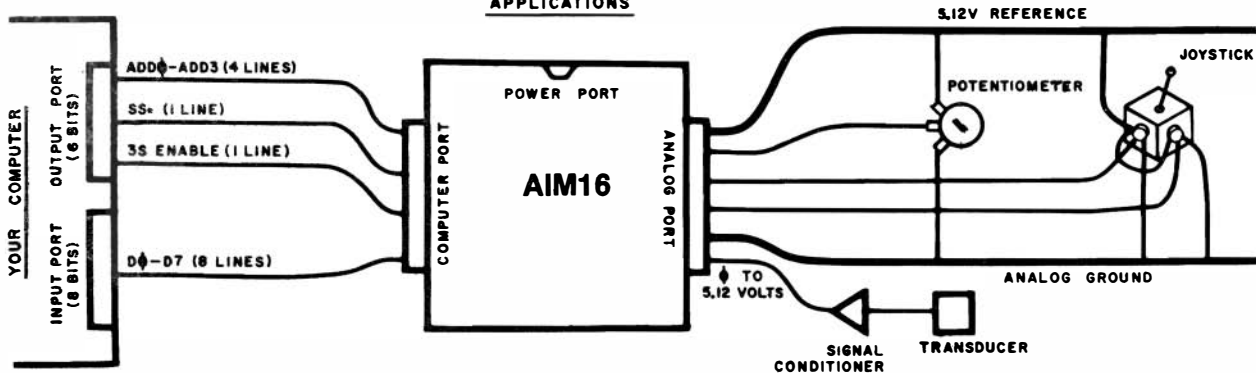
AIM 16 TIMING



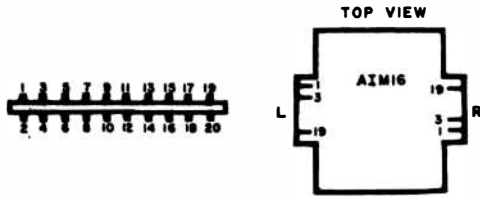
AIM 16 Timing Diagram

SYMBOL	CHARACTERISTIC	MIN	MAX	UNIT
T1	ADDX must become stable		1	microsec
T2	ADDX must remain stable	.3		microsec
T3	EOC becomes stable on D7		60	nanosec
T4	EOC is reset		100	nanosec
T5	EOC goes high indicating conversion complete		100	microsec
T6	DO-D7 becomes stable after 3S goes high		290	nanosec
T7	DO-D7 or EOC becomes stable after 3S enable goes high		290	nanosec
T8	DO-D7 or EOC enter tri-state after 3S enable goes low		290	nanosec

APPLICATIONS



PORT PIN FUNCTIONS



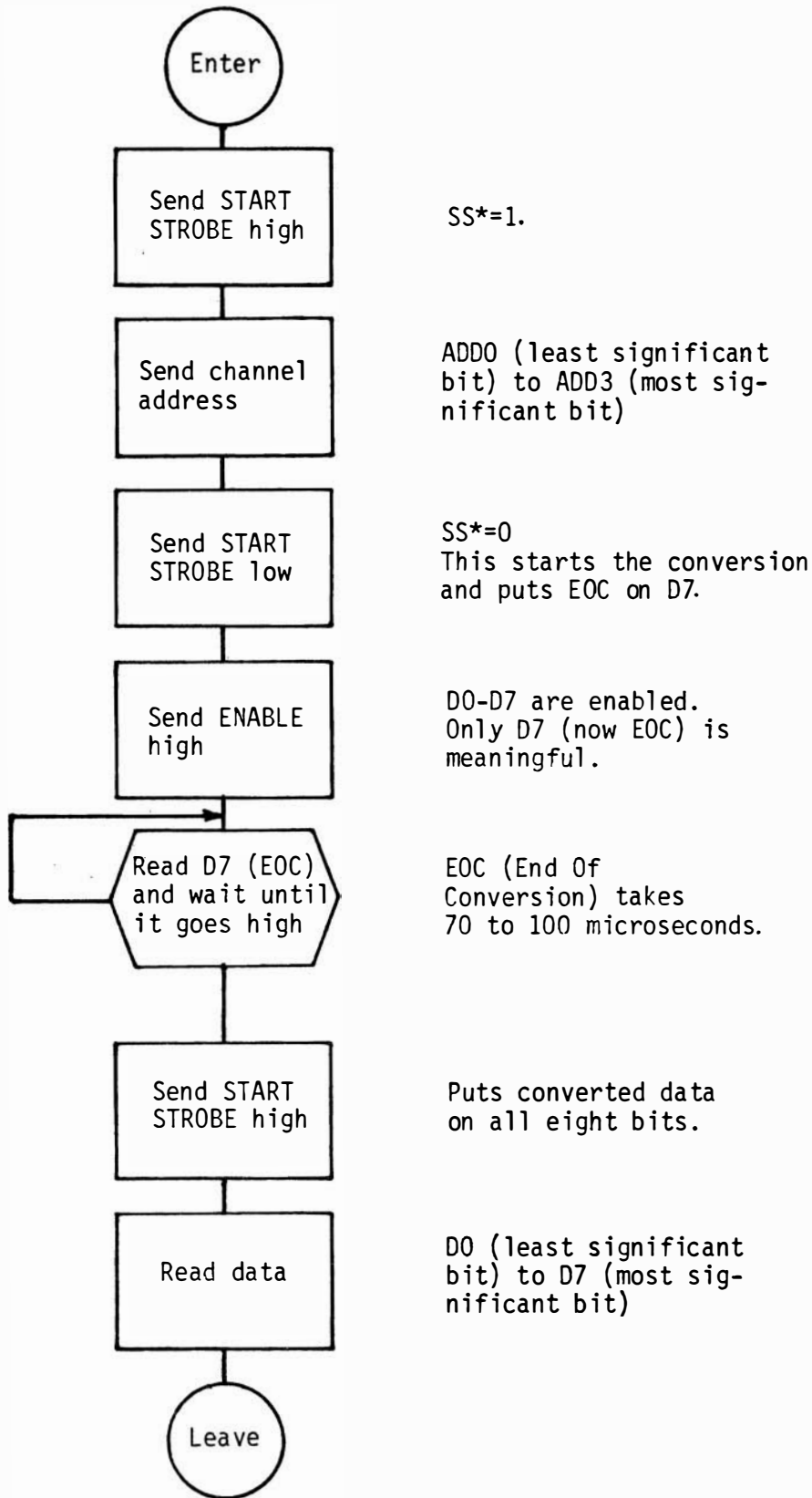
Computer Port (Connector L)

Top		Bottom	
Pin No.	Function	Pin No.	Function
1	GND	2	GND
3	D0 (LSB)	4	D4
5	D1	6	D5
7	D2	8	D6
9	D3	10	D7 (MSB), EOC
11	plus 12v	12	plus 12v
13		14	
15	3s enable	16	Start Strobe (SS*)
17	Add 0	18	Add 2
19	Add 1	20	Add 3

Analog Port (Connector R)

Top		Bottom	
Pin No.	Function	Pin No.	Function
1	GND	2	5.120 VREF
3	IN0	4	IN8
5	IN1	6	IN9
7	IN2	8	IN10
9	IN3	10	IN11
11	IN4	12	IN12
13	IN5	14	IN13
15	IN6	16	IN14
17	IN7	18	IN15
19	5.120 VREF	20	GND

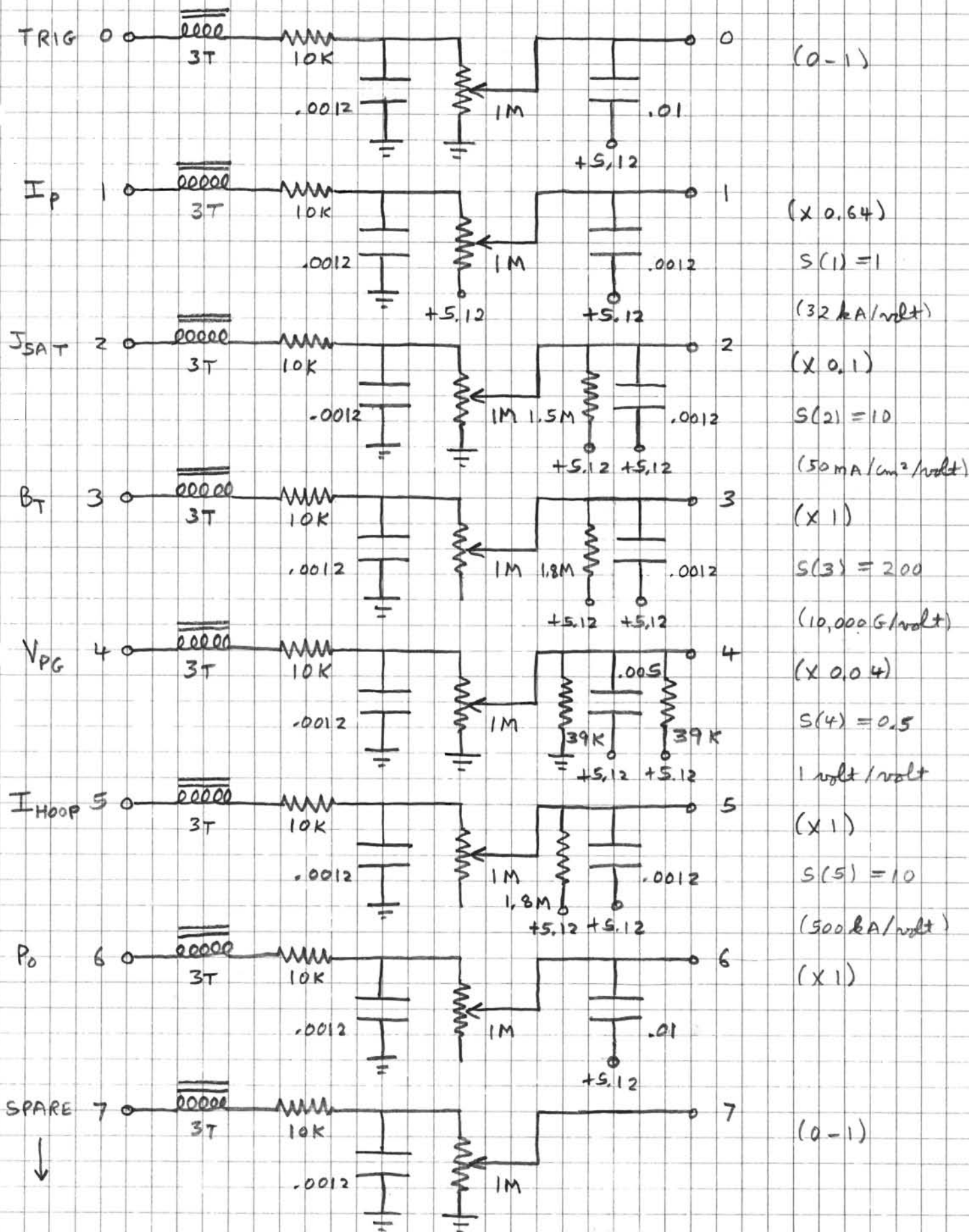
DIRECTION WITH RESPECT TO THE AIM16		COMPUTER PORT PIN FUNCTIONS	FUNCTION	LOADING OR DRIVE		
1	GND	Signal ground - tied to analog ground				
2	GND					
3	DP (LSB) out	Digital output for analog inputs.		1 TTL Load		
5	D1 out	D0 is the least significant bit. D7 is the most significant bit. A lo voltage is a logical 0. A hi voltage is a logical 1.				
7	D2 out					
9	D3 out					
4	D4 out	D7 (when SS* pin 16, is lo) is the end of conversion signal, EOC. When EOC is lo, the AIM16 is busy. When EOC is hi, the AIM16 has finished a conversion and the converted value may be read.				
6	D5 out					
8	D6 out					
10	D7 (MSB) out					
11 plus 12 volts in or out		12 volts DC power from a DAM SYSTEMS power pack or other source. If a DAM SYSTEMS power pack is used at the POWER PORT then this voltage is available to supply other DAM SYSTEMS modules. If a DAM SYSTEMS power pack is not used at the POWER PORT then a positive 12 volts (well-filtered DC) must be supplied at these pins.		60 ma in		
12 plus 12 volts in or out						
!! C A U T I O N !!						
DO NOT USE A DAM SYSTEMS POWER PACK AT THE POWER PORT WHILE POWER IS APPLIED TO THESE PINS.						
13 not used						
14 not used						
15 3S ENABLE in		Three state enable. A lo voltage disables the outputs D0-D7. a hi voltage enables D0-D7.		1 LSTTL Load		
16 SS* in		Start Strobe not. A hi to lo transition resets the AIM 16 and starts the conversion of the analog input selected by the digital inputs on pins 17 to 20. While SS* remains lo, and the 3S ENABLE is hi, the EOC (End of Conversion) signal appears on pin 10. When is SS* is hi, and the 3S ENABLE is hi, D7 is on pin 10 and D0 to D6 are on pins 3 to 9. respectively.		1 LSTTL Load		
17 ADD0 in		Address lines - select the analog input to be converted according to the following table:		Vin(hi)-3.5 volts min		
19 ADD1 in				Vin(lo)-1.5 volts max		
18 ADD2 in						
20 ADD3 in						
		Analog input	ADD3	ADD2	ADD 1	ADD 0
		IN0	lo	lo	lo	lo
		IN1	lo	lo	lo	hi
		IN2	lo	lo	hi	lo
		IN3	lo	lo	hi	hi
		IN4	lo	hi	lo	lo
		IN5	lo	hi	lo	hi
		IN6	lo	hi	hi	lo
		IN7	lo	hi	hi	hi
		IN8	hi	lo	lo	lo
		IN9	hi	lo	lo	hi
		IN10	hi	lo	hi	lo
		IN11	hi	lo	hi	hi
		IN12	hi	hi	lo	lo
		IN13	hi	hi	lo	hi
		IN14	hi	hi	hi	lo
		IN15	hi	hi	hi	hi

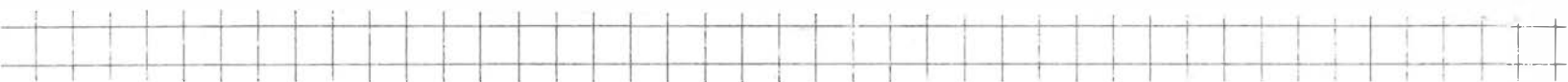


Flowchart for reading one channel of data from the AIM16.

APPENDIX D

Schematic of A-to-D Input Circuit





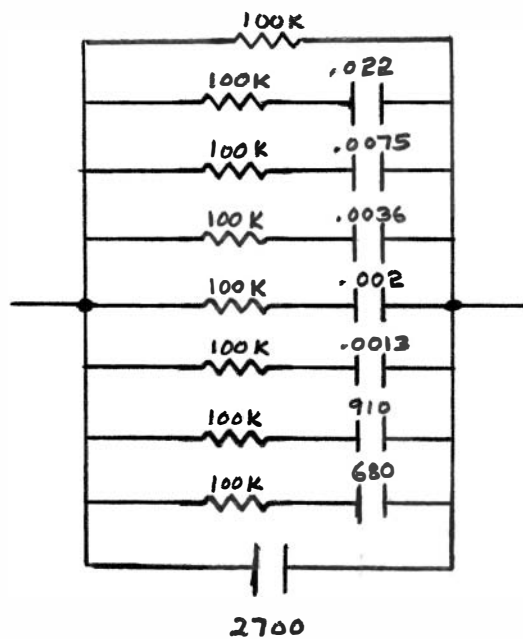
APPENDIX F

Schematic of Circuit to Model Hoop Resistance

$$Z = Z_{DC} \left[1 + \sum_{i=1}^{\infty} e^{-t/\tau_i} \right]$$

$$R_i = 100 \text{ k}\Omega$$

<u>i</u>	<u>τ_i (msec)</u>	<u>C_i (pF)</u>
1	2.43	24300
2	.73	7300
3	.35	3500
4	.2	2000
5	.132	1320
6	.0979	929
7	.0690	690
8	.0533	533
9	.0424	424
10	.0345	345
11	.0287	287
12	.0242	242
13	.0207	207
14	.0189	189
15	.0156	156
16	.0137	137
17	.0122	122
18	.0109	109
19	.0098	98
10	.0088	88
$\sum_{i=1}^{\infty} \tau_i =$	4.27	42700



AIM16 Data Sheet Excerpts

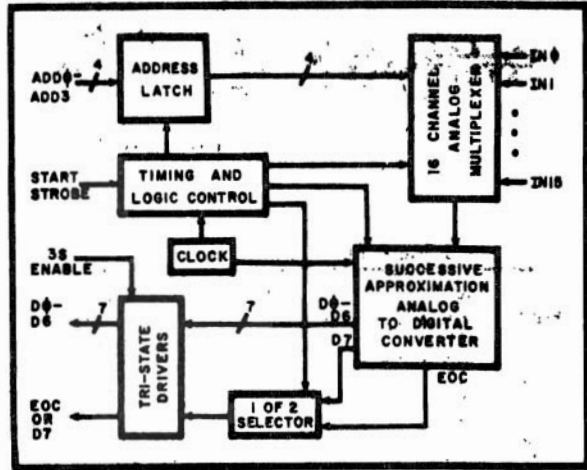
AIM16 DATA SHEET

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Conversion data -
 T_c - conversion time, per channel: 100 microsec max, 80 typ
 counts per channel: 256
 output range (each channel): 00-FF (hex)
 0-255 (decimal)
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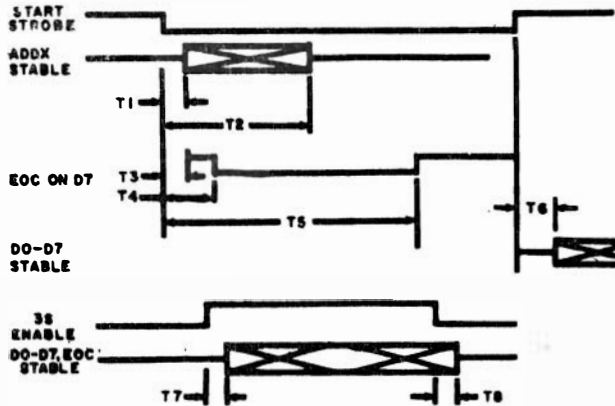
Absolute maximum error: .7%
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AIM16 BLOCK DIAGRAM

AIM 16 TIMING



AIM 16 Timing Diagram

SYMBOL	CHARACTERISTIC	MIN	MAX	UNIT
T1	ADDX must become stable		1	microsec
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T3	EOC becomes stable on D7		60	nanosec
T4	EOC is reset		100	nanosec
T5	EOC goes high indicating conversion complete		100	microsec
T6	DO-D7 becomes stable after SS goes high		290	nanosec
T7	DO-D7 or EOC becomes stable after 3S enable goes high		290	nanosec
T8	DO-D7 or EOC enter tri-state after 3S enable goes low		290	nanosec

APPLICATIONS

